Analysis of Friction Clutch plate using FEA

P.Naga Karna¹, Tippa Bhimasankara Rao²

¹PG Student, Department of Mechanical Engineering, Nimra Institute of Science and Technology
²HOD, Department of Mechanical Engineering, Nimra Institute of Science and Technology, Vijayawada, AP, INDIA

Abstract:- The object of the present work is to observe the stress distribution and the temperature distribution of the clutch plate by changing the material. And for that we are taken one existing clutch plate dimensions and modeled it by using Pro-e after analysis is done by using Ansys. Here we have done two types of analyses on clutch plate namely static analysis and thermal analysis. By performing these analyses we got the results namely stress distribution and temperature distribution. Finally we compare the results steel and aluminium wet clutch plates.

Keywords:- Analysis, modeling, static analysis, thermal analysis.

I. INTRODUCTION

A clutch is that part of engine which engages or disengages power from the engine crankshaft to transmission. A clutch is mechanism by which you change the gears. In simple words, it turns on or off power to rear wheel. A clutch is made of clutch assembly which includes clutch plate, Clutch basket, Clutch hub, pressure plates, Clutch springs, lever and clutch cable. A clutch in which there is provided a clutch disc having clutch facings made of cerametallic or like material, a flywheel having a friction surface to be brought into frictional contact with one of the facings, and a pressure plate supported by a clutch cover for conjoint rotation with the flywheel and urged in a direction to press the facing against the flywheel, with the pressure plate having a friction surface to be brought into frictional contact with the other facing. Segments made of heat-treated hard steel plate are fixed to each of the flywheel and the pressure plate to provide the friction surface thereof.

Clutch Engaged/Disengaged – On most motorcycles, the clutch is operated by the clutch lever, located on the left handlebar. No pressure on the lever means that the clutch plates are engaged (driving), while pulling the lever back towards the rider will disengage the clutch plates, allowing the rider to shift gears. There are several types of clutch plates available which are divided into external and internal tooth and the most commonly used materials for the clutch plates are steel and for friction material cerametallic or like material which is named as Kevlar and it is a composite material.

II. CLUTCH PLATE

A clutch plate is part of series of discs inside of a transmission. The clutch plate is round and has a friction sensitive surface that allows it to grip. It sits next to the fly wheel, which is connected to the drive shaft permanently. That means the flywheel immediately starts to spin as soon as the engine is turned on and the motor turns the crankshaft. When this happens in a manual transmission, the clutch must be disengaged. That is, it is pulled back from the flywheel, so it can spin without engaging the wheels.

Fig.1 Clutch Plates
III. TYPES OF CLUTCH PLATES

- **Wet Clutch**
  Wet clutch are universal and found on any bike. Almost 99% of motorcycle manufactured uses this kind of clutch. In the wet clutch set up the entire clutch is inside the case of the bike. Here it is bathed in oil which acts like a kind of dampener. It stops the clutch from knocking on itself.

- **Dry Clutch**
  The dry clutch is almost identical to the wet clutch the only difference s there are seals on the shafts that keep oil out. In the dry clutch set up the entire clutch is outside the case of the bike. There is no oil circulated in to the clutch, which result into clutch knocking on itself. Ducati’s are almost the

IV. CLUTCH PLATE MANUFACTURING PROCEDURE

- **First type**
  Concurrently as seen in FIG.2 the remaining line of cut segments 14b-z advances the second segment 14b to the transfer position 71 in the shuttle assembly 70. the shuttle assembly 70 engages the second keystone segment 14b and moves in a reverse direction and transfer the second segment 14b in to a first empty pocket 97 of the adjacent second indexing fixture 92. The second indexing fixture 92 is located opposite, or at a180 degrees, from the first indexing fixture 91. Continuing with the assembly steps, the first indexing fixture 91 rotates to its next, or second, there by exposing another, or second, empty pocket, for case of illustration, each pocket will generally be referred to as 96 or 97. But it should be understood that the no. of pockets. In each indexing fixture is depended up on the no. of key stone. Friction segments that are desired on the friction plate. The shuttle assembly 70 again reverse direction, engages a third key stone segment 14c, now beginning moved in to the transfer position 71, and transfer the third segment 14c in to the second pocket 96 in the first indexing fixture 91. Concurrently, the second indexing fixture 92 rotates one position there by exposing another, or second empty pocket for receiving the fourth cut segment 14d. The sequence of alternating placements of key stone statement segments continues until all the pockets 96 and 97 in both the first 91 and second 91 indexing fixtures have been filled with key stone segment 14.

![Fig.2](image)

- **Second type**
  Referring now to Fig.3, a plan view of the indexing fixture 91 is shown; the direction of travel is indicated by arrow z of alternating segments 14a, 14c, 14e and 14g travelling along the bottom track 74. The indexing fixture 91 comprises an indexing plate 94 having a plurality of integrally machined segment pockets 96. In the embodiment shown, there are 20 segments pockets in the indexing plate 94. However, it should be understood that the indexing plate 94 can have different no. of pockets, depending on the no. of individual segments to be positioned on a core plate. It should be further understood that the second indexing figure 92 can be substantially identical to the first indexing figure 91 will be described in detail herein. It should be further understood however, that such description also adequately describes the second indexing figure 92.

  The pockets 96 are slightly recessed in the indexing plate 94 to allow for accurate, vertical, radial and circumferential location of each segment 14. In certain embodiments, the depth of the pockets 96 ranges from about 0.020 to about 0.030 inches. Further, the key stone or trapezoidal, shape of the segment facilities accurate positioning of each segment 14 in the corresponding pocket 96. Each pocket 96 defines a separate vacuum port 98. Typically, the cut segments have an adhesive or glued bracking such that the porosity of the cut segment is relatively low, therefore, the vacuum port 98 is used to apply a vacuum to further maintain the positioning of the segment 14 in the pocket 96 (if required). In the embodiment shown, the indexing plate 94 is operatively connected to a rotating mechanism generally indicated as 100 which rotates, or indexes, the indexing plate 94 in the case of a 20-cut segment core plate, for instance, the indexing figure 91 is moved or indexed 18 degrees
between the placement of segments since indexing accuracy is important, the rotating apparatus 100 generally comprises a servo motor and gear head assembly (not shown) which is operatively mounted to the indexing fixture 91. Once the pockets 96 have been filled with segments 14a-t, the segments are transferred to abounding nest 140 in a suitable manner.

![Figure 3: Second type of Clutch plate manufacturing](image)

**V. ARRANGEMENT OF CLUTCH PLATES**

FIG: 4 is vertical cross sectional view of a whole of a multiple disc friction clutch. In FIG: 1, the multiple disc friction clutch is arranged between a crank shaft 1 and an input shaft 2 of a gear transmission 3 in a power transmission path from an engine (not shown) of a motor cycle to a rear wheel (not shown), and is provided with a clutch outer member 4 for take in power into the clutch, a clutch hub 5 for takeout power from the clutch, a clutch output shaft 8 integrally formed with the input shaft 2, a clutch output tube shaft (rotating member) 9 spline fitted to an outer peripheral surface of the clutch output shaft 8 in such a manner as to be immovable in an axial direction of the clutch output shaft 8, a plurality of input friction plates 10 and output friction plates 11 arranged between the clutch outer member 4 and the clutch hub 5, a pressing member (a pressure plate or a pusher plate) 12 pressing both the friction plates 10 & 11 in an axial direction of the clutch output shaft 8 (in other words an axial direction of the tube shaft 9), and coil shaped clutch spring 15 applying a pressing load to the pressing member 12. Further, in addition to each of the member for pressing or the like, there is provided a movable coupling hub 16 which is utilized for both of a pressing load increasing mechanism and a back torque limiter mechanism mentioned below, as well as transmitting a torque between the clutch hub 5 and the tube shaft 9. A shift output shaft (not shown) of the gear transmission 3 is coupled to the rear wheel in an interlocking manner, for example via a chain transmission mechanism.

![Figure 4: Arrangement of clutch plates](image)

**VI. CLUTCH PLATE DIMENSIONS**

- Addendum circle diameter = 63mm
- Dedendum circle diameter = 60mm
- Inner circle diameter = 51.2mm
- Tooth width = 3mm
Fig.5:- Dimensions of tooth profile and friction material profile

- Tooth height = 1.5mm
- Tooth thickness = 2mm
- Friction material dimensions:
  - Height = 4mm
  - Width at top =4mm
  - Width at bottom = 3.5mm
  - Depth=2mm

VII. IDENTIFIED MATERIAL PROPERTIES FOR CLUTCH PLATE

- **Aluminium**
  - Density: 2.70g/cm$^3$
  - Thermal conductivity: 300k or 237wm$^{-1}$k$^{-1}$
  - Young’s modulus: 70gpa
  - Shear modulus: 26gpa
  - Bulk modulus: 76gpa
  - Poisson’s ratio: 0.35
  - Alpha: 10cm$^2$/sec
  - S m: 37gpa

- **Steel**
  - Density: 7.85 kg/m$^3$
  - Thermal conductivity: 11.2-36. W/m-K
  - Young’s modulus: 200gpa
  - Poisson’s ratio: 0.27-0.3

- **Kevlar is the friction material**
  Kevlar can be known as fibre reinforced polymers.
  - Kevlar has density 1440g/m$^3$ and
  - Modulus of rigidity: 200-300gpa.

VIII. MODELING OF CLUTCH PLATE USING PRO-E

For modeling of a clutch plate we used the PRO-ENGINEERING, it was developed by parametric technology corporation, USA and its latest version is PRO-E WILDFIRE.4 The RAM requirement for this software is 256MB and OS requirement to operate in WINDOWS 98/2000.

**Procedure of Modeling of spur gear in Pro-E:-**

- Start → All programs → PTC→ Pro-E→ Pro-E
- Select the Part module and change the dimensions in to mm
- Drawn the first base circle
- Extruded the base circle up to required width
- Select the sketch and select the surface of the base circle
- Drawn the teeth and extruded up to the same width
- By using pattern command in Pro-E generated the required number of teeth
IX. THE GENERATED MODEL OF CLUTCH PLATE USING PRO-E

The generated model of clutch plate using Pro-E

Fig.6: Sketch of Clutch plate model in Pro-E  Fig.7: Solid model  Fig.8: Wire frame model

X. ANALYSIS OF CLUTCH PLATE USING ANSYS

For doing analysis on the clutch plate we used the ANSYS package, it is a general purpose finite element modeling package for numerically solving a wide variety of mechanical problems.

Procedure of the analysis of the gear by using Ansys package:-
- Start → All programs → Ansys 8.0 → Ansys
- Move the mechanical tool bar (for easy doing of the analysis)
- Select the Ansys model i.e. static or modal, structural or thermal, and specify the dimensions that are used in the modeling, and give the analysis name
- Move to setup mode to the model mode import the IGES file of that clutch plate
- Apply the material properties and mesh the object
- After meshing move to the loads menu and constrain the inner circle that is lie on the shaft.
- Apply the loads on the clutch plate
- Click on Solve now Seen the results.

XI. RESULTS FOR ALUMINIUM CLUTCH PLATE

- Static analysis

Fig.9: Ansys model  Fig.10: Meshed model

Fig.11: Displaced shape  Fig.12: Static equivalent stress
TABLE 1: Static analysis table for aluminum

<table>
<thead>
<tr>
<th>Environment Name</th>
<th>Solve OK?</th>
<th>Maximum Displacement (mm)</th>
<th>Maximum Equivalent Stress (MPa)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Environment 1</td>
<td>Yes</td>
<td>0.1697E-03</td>
<td>3.8230</td>
</tr>
</tbody>
</table>

- **Thermal analysis**

Fig. 13: Thermal flux  
Fig. 14: Thermal gradient

**XII. RESULTS FOR STEEL CLUTCH PLATE**

- **Static analysis**

Fig. 15: Displaced shape  
Fig. 16: Static equivalent stress

<table>
<thead>
<tr>
<th>Environment Name</th>
<th>Solve OK?</th>
<th>Maximum Displacement (mm)</th>
<th>Maximum Equivalent Stress (MPa)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Environment 1</td>
<td>Yes</td>
<td>0.63736E+04</td>
<td>4.1632</td>
</tr>
</tbody>
</table>

**Table 2**: Static analysis table for steel

- **Thermal analysis**

Fig. 17: Thermal flux  
Fig. 18: Thermal gradient

---

86
XIII. CONCLUSION

The design, modeling and analysis of clutch plate is done. It is observed that the same required output dimensions of clutch plate are various with respect to the material. The conclusion is that for the steel material the stress intensity and displaced shape results are better than aluminium in static analysis and in thermal analysis also for the steel material the thermal flux and thermal gradient are better than aluminium. We came to know that steel is the best material for clutch plate and it will be replaced by any other composite material or an alloy or a reinforced material.

ACKNOWLEDGMENT

I would like to thank my Guide, Mr. Tippa Bhimasankara Rao for his time and support. In addition, I would like to thank my friends for sharing their experience in PRO-E, ANSYS. Finally, I would like to thank my family for their support and putting up with me for these past few months moral and financial support during my studies.

REFERENCES

[8] www.cs.cmu.edu/People/rapidproto/mechanisms/references.html
[12] Analysis and approximation of contact problem
[13] By Mircea Sofonia and Weimin Hann
[14] Elastic contact analysis by boundary elements
[15] By Susumu Takahashi
[16] “A comprehensive analysis of fillet and contact stresses in straight spur gears”
[17] By M.A. Alfares